

ELABORATION OF A TENDENCY MODEL AND DETERMINATION OF OPTIMAL FEED RATE PROFILES OF STYRENE / BUTYL ACRYLATE SEMI-BATCH EMULSION COPOLYMERIZATION REACTOR

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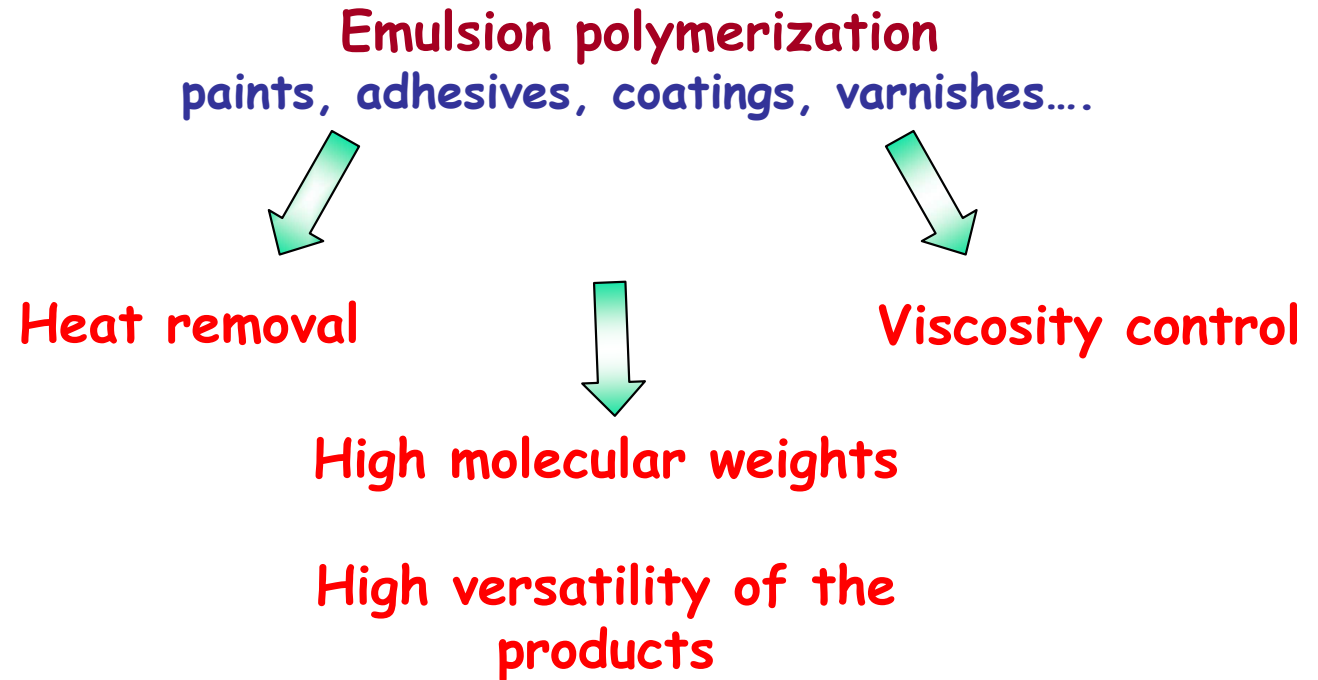
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SUMMARY

- ◆ **INTRODUCTION**
- ◆ **PROCESS MODEL**
- ◆ **EXPERIMENTAL SET-UP**
- ◆ **PARAMETRS IDENTIFICATION**
- ◆ **MODEL VALIDATION**
- ◆ **MULTICRITERIA OPTIMIZATION**
- ◆ **CONCLUSIONS AND FUTURE TRENDS**

- ◆ Introduction
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- ◆ Conclusions /futur trends



Position of the problem

Tendency model



Molecular weight distribution (MWD)
Glass transition temperature (T_g)
Particle size distribution (PSD)...

Parameter identification
and model validation



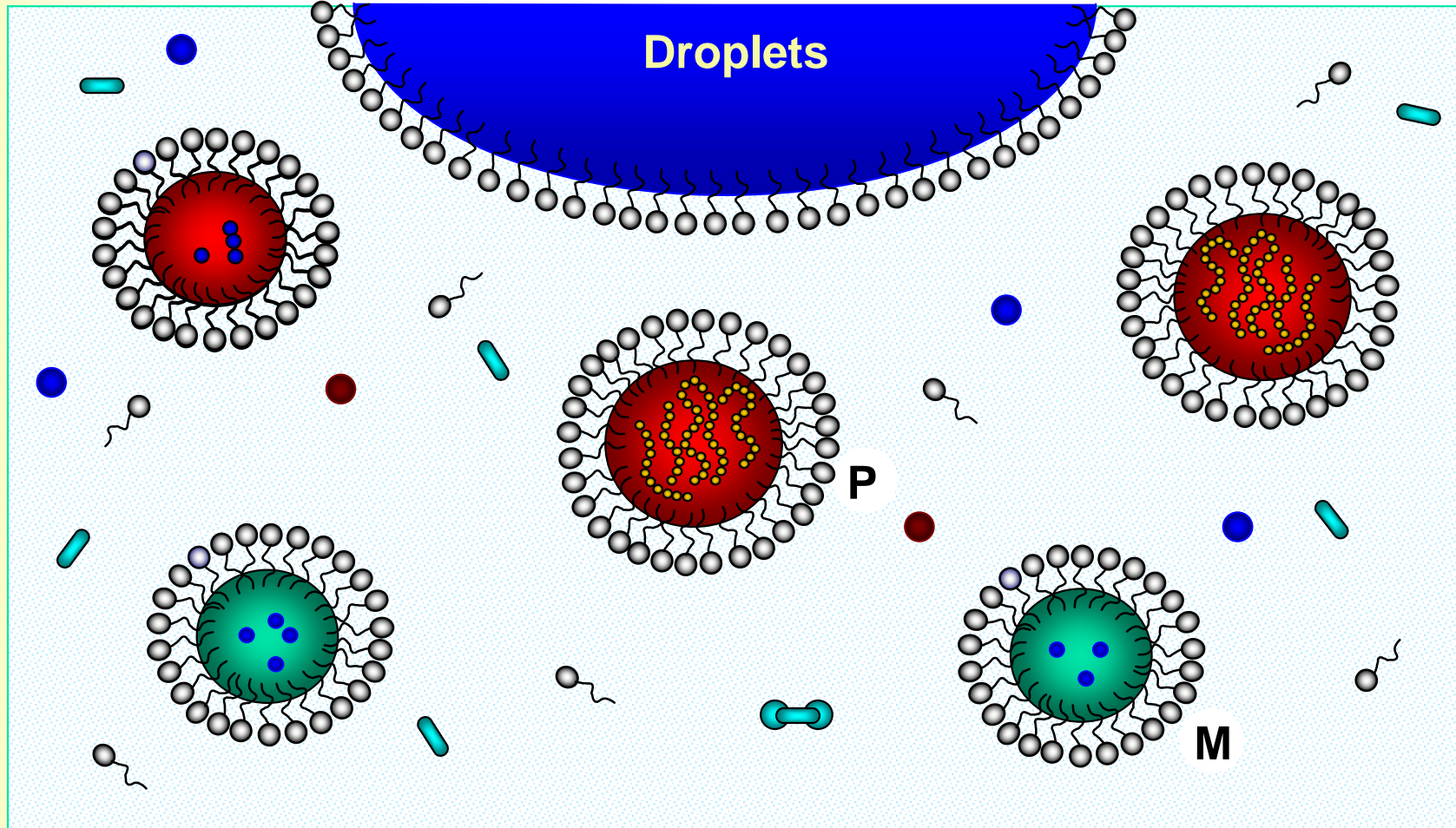
The end-use
properties of the
products

Multiobjective optimization



- *Rheological properties*
- *Adhesion and film-forming properties*
- *Elasticity, strength, toughness, and solvent resistance*

PRINCIPLE : Harkins' theory



: Micelle



: Particle



: Surfactant



: Free radical



: Initiator



: Monomer

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◆ Step 1 : Nucleation

Micellar or homogeneous
Number of particles $N_p \uparrow$

Conversion : 0 - 10 %



Few minutes



**Micelles
disappearance**

◆ Step 2 : Particles growth

N_p : constant
Particles saturated with monomer

Conversion : 10 - 40 %



**Droplets
disappearance**

◆ Step 3 : End of polymerization

Particles unsaturated

Conversion : 40-100 %

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Main assumptions

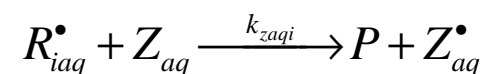
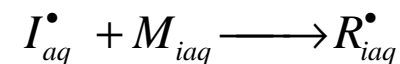
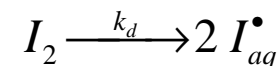
- ➔ Only micellar nucleation is considered.
- ➔ Propagation, chain transfer to monomer, transfer chain transfer agent to monomers, and termination reactions in the aqueuse phase are neglected (weak solubility in water).
- ➔ Radical desorption is considered
- ➔ Droplets and particles diameters are considered as monodisperse
- ➔ The reactor is perfectly mixed and isothermal

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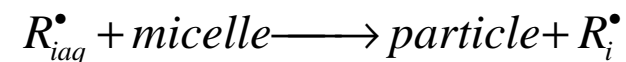
Reactions Scheme

Aqueous phase

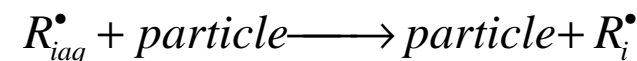
Initiation



Inhibition



Nucleation



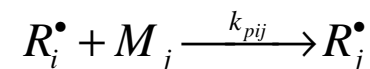
Radical absorption

Radical desorption

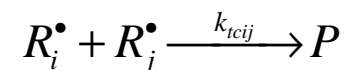


Organic phase

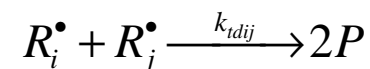
Propagation



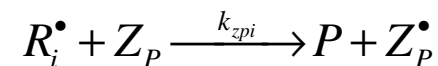
Term. by combination



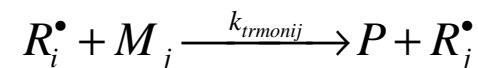
Term. by disproportionation



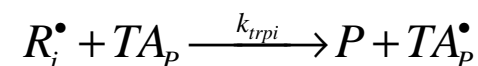
Inhibition

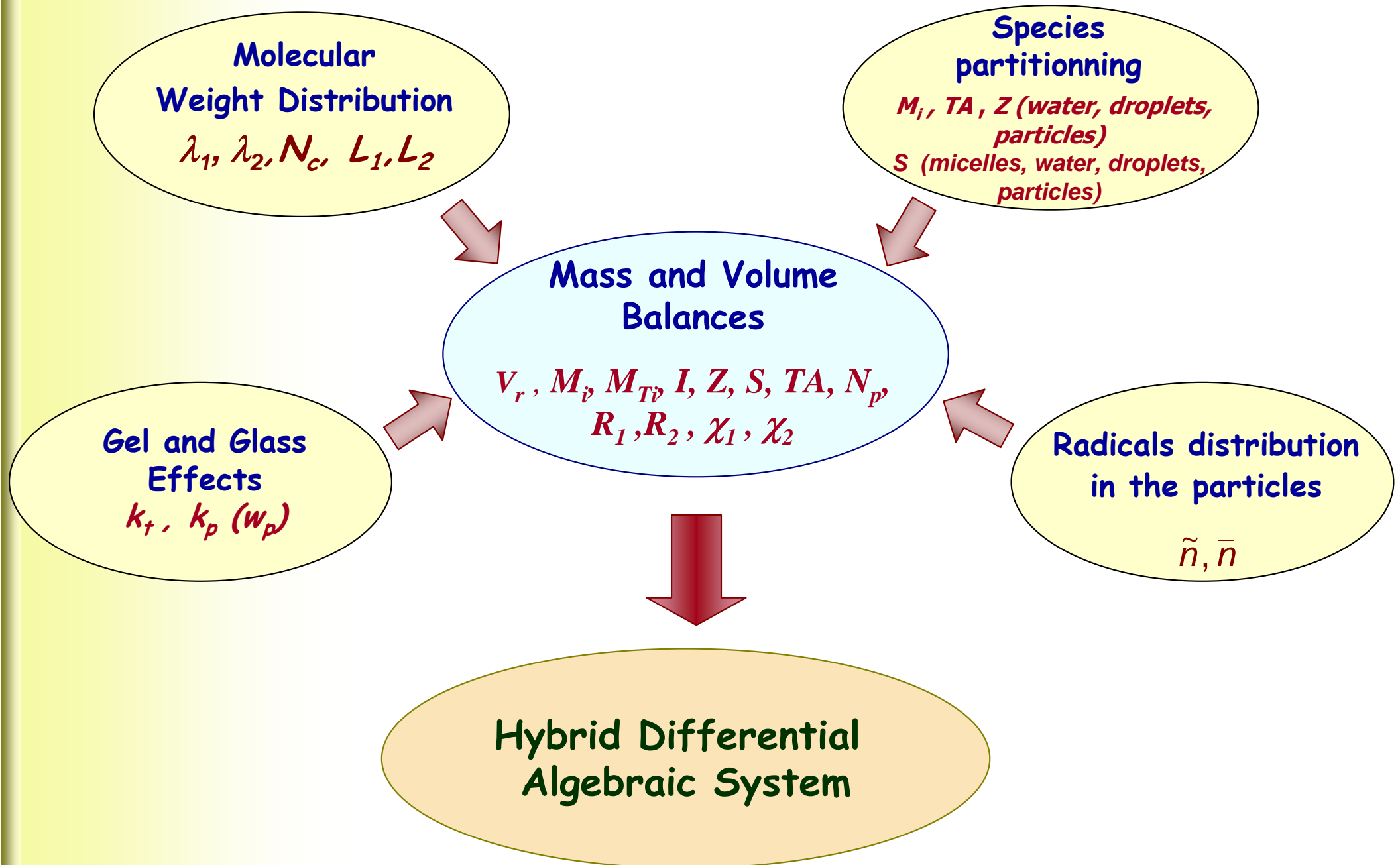


Transfer to monomers



Transfer CTA-monomers





Material balance

$$\frac{dV_{aq}}{dt} = Q_{aqf}$$

$$\frac{dV_R}{dt} = Q_f + \sum_{i=1,2} \left(\frac{1}{\rho_{pi}} - \frac{1}{\rho_i} \right) M_M^i (\mathfrak{R}_{pi} + \mathfrak{R}_{trmi})$$

$$\frac{dM_i}{dt} = -\mathfrak{R}_{pi} - \mathfrak{R}_{trmi} + Q_{Mif}$$

$$\frac{dM_{Ti}}{dt} = Q_{Mif}$$

$$\frac{dI}{dt} = -\mathfrak{R}_d + Q_{If}$$

$$\frac{dZ}{dt} = -\mathfrak{R}_{Zaq} - (\mathfrak{R}_{Zp1} + \mathfrak{R}_{Zp2}) + Q_{Zf}$$

$$\frac{dTA}{dt} = -\mathfrak{R}_{TAp1} - \mathfrak{R}_{TAp2} + Q_{TAf}$$

$$\frac{dS}{dt} = Q_{Sf}$$

$$\frac{dN_p}{dt} = \mathfrak{R}_N$$

$$\begin{aligned} \frac{dR_1}{dt} = & (\mathfrak{R}_N + \mathfrak{R}_{cp}) \frac{M_1}{M_1 + M_2} - \mathfrak{R}_{p12} + \mathfrak{R}_{p21} - \mathfrak{R}_{trm12} \\ & + \mathfrak{R}_{trm21} - \mathfrak{R}_{Zp1} - \mathfrak{R}_{des1} - \mathfrak{R}_{TAp1} - (\mathfrak{R}_{T11} + \mathfrak{R}_{T12}) \end{aligned}$$

$$\begin{aligned} \frac{d(N_p \bar{n} \chi_1)}{dt} = & (\mathfrak{R}_N + \mathfrak{R}_{cp}) \frac{M_1}{M_1 + M_2} - \mathfrak{R}_{trm21} + \mathfrak{R}_{trm11} \\ & - \mathfrak{R}_{des1} - (\mathfrak{R}_{trm11} + \mathfrak{R}_{trm12} + \mathfrak{R}_{p11} + \mathfrak{R}_{p12} + \mathfrak{R}_{TAp1} \\ & + \mathfrak{R}_{Zp1}) \chi_1 - (\mathfrak{R}_{T11} - \mathfrak{R}_{T12}) \chi_1 \end{aligned}$$

Populations balance

$$\frac{d(N_p \bar{n})}{dt} = \mathfrak{R}_N + \mathfrak{R}_{cp} - (\mathfrak{R}_T + \mathfrak{R}_{Zp} + \mathfrak{R}_{des} + \mathfrak{R}_{TAp})$$

$$\frac{d(N_p \tilde{n})}{dt} = 2\mathfrak{R}_{cp} \bar{n} + \left(\frac{2\tilde{n}}{\bar{n}} + 1 \right) \mathfrak{R}_T - 2\frac{\tilde{n}}{\bar{n}} (\mathfrak{R}_{Zp} + \mathfrak{R}_{des} + \mathfrak{R}_{TAp})$$

Equations of Moments

$$\begin{aligned} \frac{d(N_p \bar{n} \lambda_1)}{dt} = & \mathfrak{R}_N + \mathfrak{R}_{cp} - \mathfrak{R}_{des} + \mathfrak{R}_P + \mathfrak{R}_{trm} (1 - \lambda_2) \\ & - (\mathfrak{R}_{Zp} + \mathfrak{R}_T + \mathfrak{R}_{TAp}) \lambda_1 \end{aligned}$$

$$\begin{aligned} \frac{d(N_p \bar{n} \lambda_2)}{dt} = & \mathfrak{R}_N + \mathfrak{R}_{cp} - \mathfrak{R}_{des} + \mathfrak{R}_P (1 - 2\lambda_1) + \mathfrak{R}_{trm} (1 - \lambda_2) \\ & - (\mathfrak{R}_{Zp} + \mathfrak{R}_T + \mathfrak{R}_{TAp}) \lambda_2 \end{aligned}$$

$$\frac{d(N_C)}{dt} = \mathfrak{R}_N + \mathfrak{R}_{cp} + \mathfrak{R}_{trm} - \mathfrak{R}_{des} + \frac{\mathfrak{R}_{TC}}{2}$$

$$\frac{d(N_C L_1)}{dt} = \mathfrak{R}_N + \mathfrak{R}_{cp} + \mathfrak{R}_{trm} + \mathfrak{R}_P - \mathfrak{R}_{des}$$

$$\frac{d(N_C L_2)}{dt} = \mathfrak{R}_N + \mathfrak{R}_{cp} + \mathfrak{R}_{trm} + \mathfrak{R}_P (1 - 2\lambda_1) - \mathfrak{R}_{TC} \lambda_1^2 - \mathfrak{R}_{des}$$

Algebraic equations

$$V_p = \frac{\sigma}{\sigma - 1} V_{pol}$$

$$\begin{aligned} \frac{1}{\sigma} = & \frac{Z M_M^Z}{\rho_Z (V_p + V_d \sigma + V_{aq} K_{pZ})} + \frac{T A M_M^{TA}}{\rho_{TA} (V_p + V_d \sigma + V_{aq} K_{pTA})} \\ & + \sum_{j=A,B} \frac{M_j M_M^j}{\rho_j (V_p + V_d \sigma + V_{aq} K_{aq-p}^j)} \end{aligned}$$

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Application : Styrene / Butyl acrylate

Recipe :

Dispersion medium	: Water	68 %
Monomer 1 (M1)	: Butyl Acrylate	} 29.8 %
Monomer 2 (M2)	: Styrene	
Surfactant (S)	: REWOPOL SBFA 50	2 %
Initiator (I)	: Ammonium persulfate	0.1 %
Chain Transfer Agent (TA)	: n-C12 mercaptan	0.1 %

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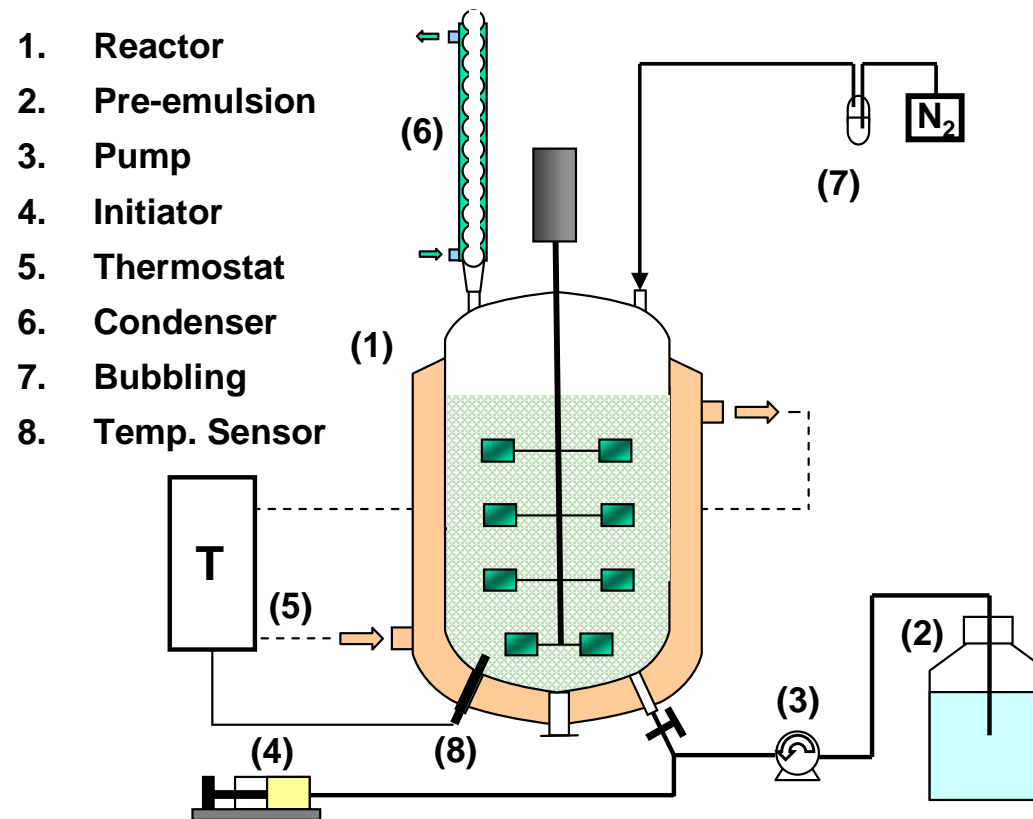
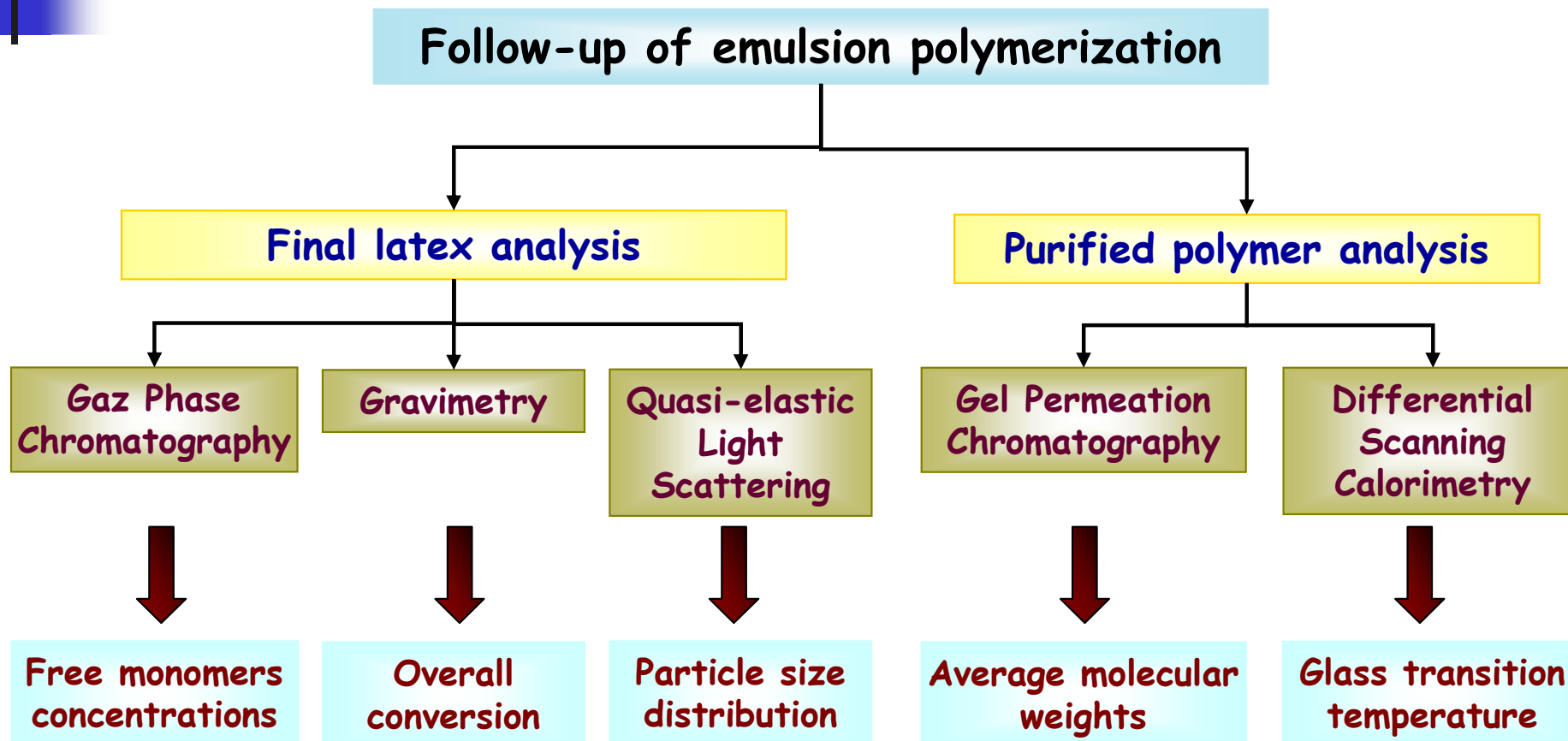


Diagram of the reactor

Experimental investigation



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Number of parameters to be determined: 38

Identified parameters : 18 parameters from an estimability ranking technique (Zhen et al., 2003) (the other parameters were taken from literature)

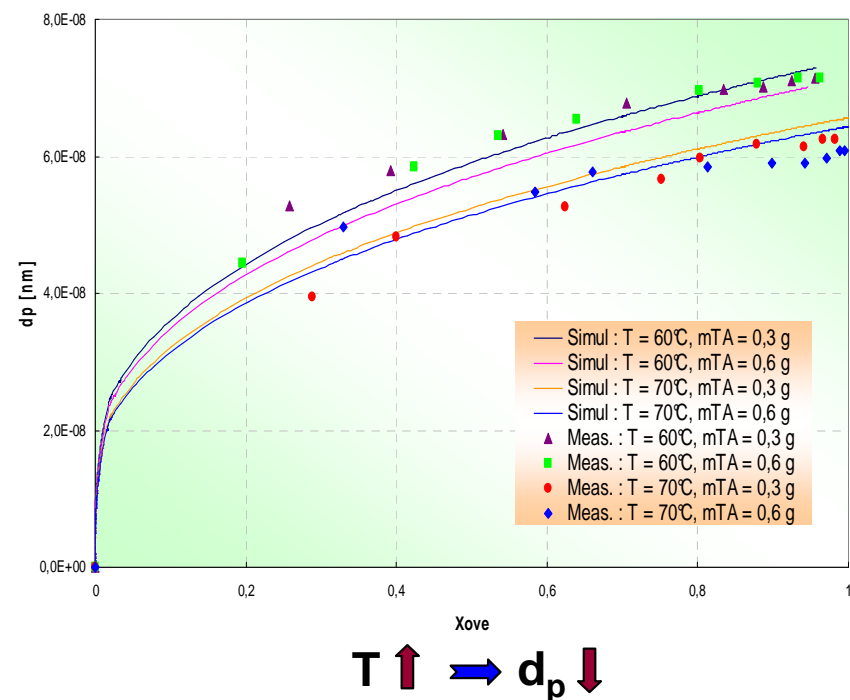
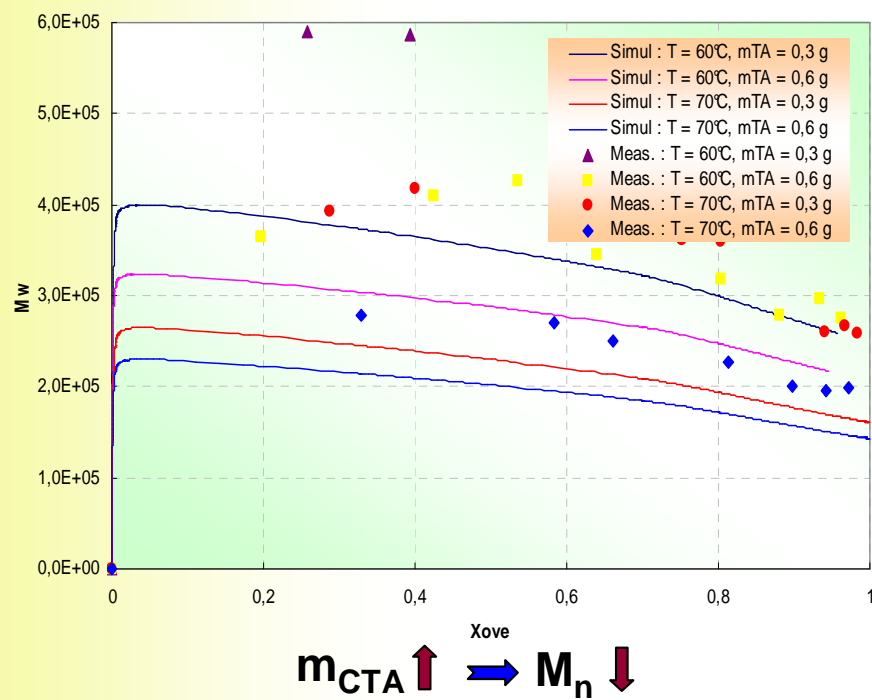
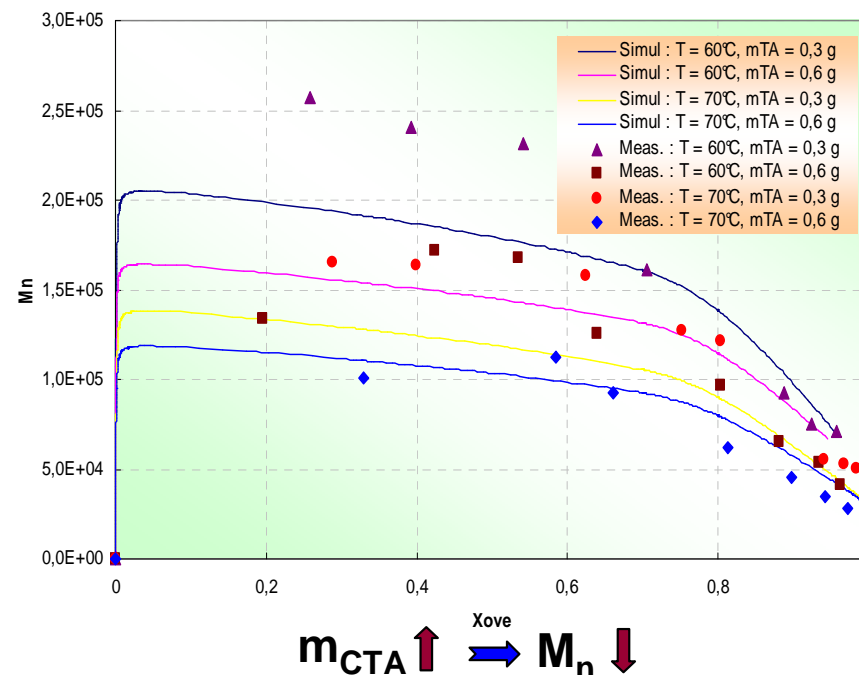
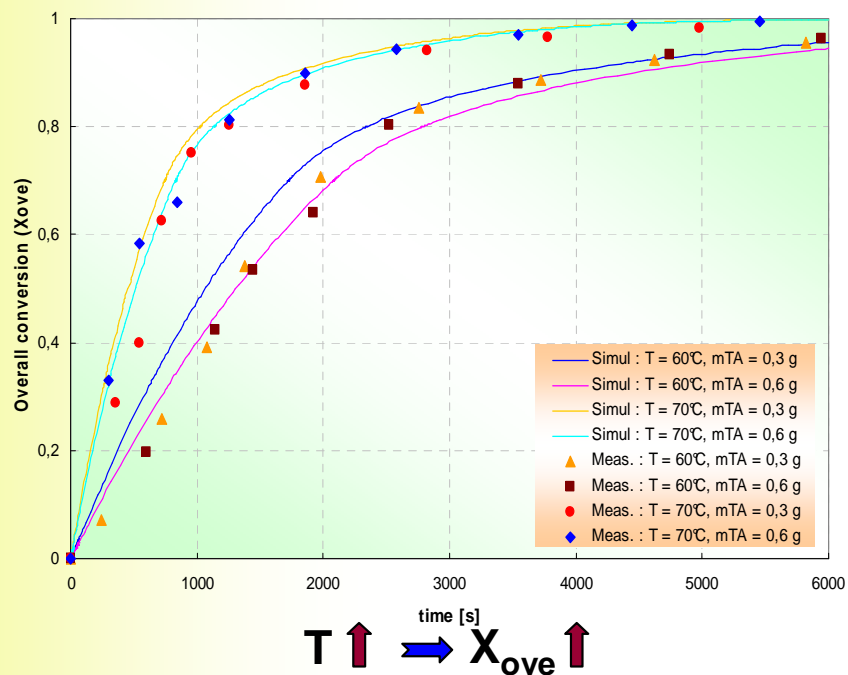
Experimental data : X, Mn, Mw, dp, Res. Monomers

Criteria of optimization : maximum likelihood

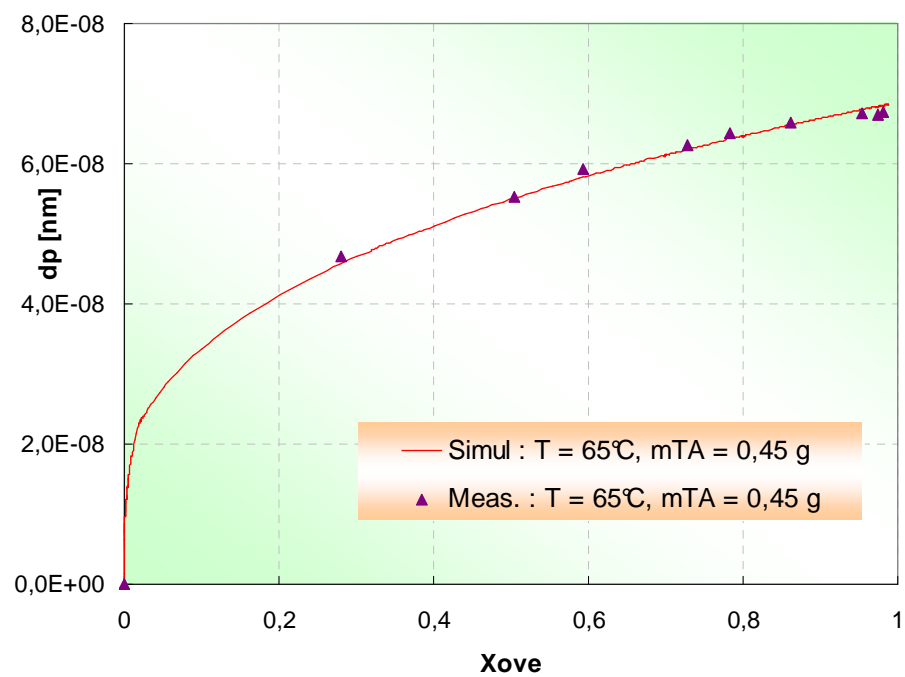
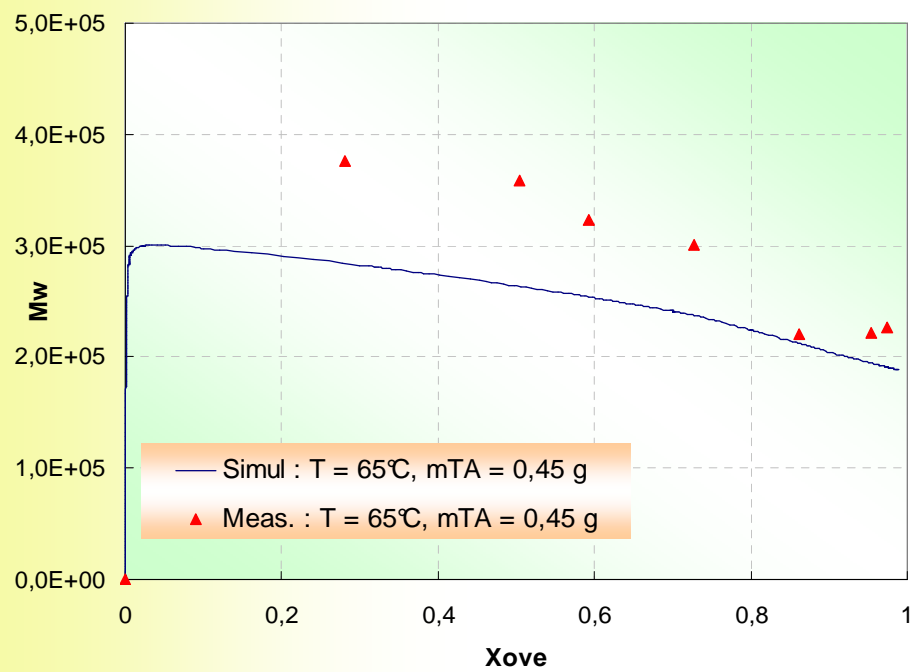
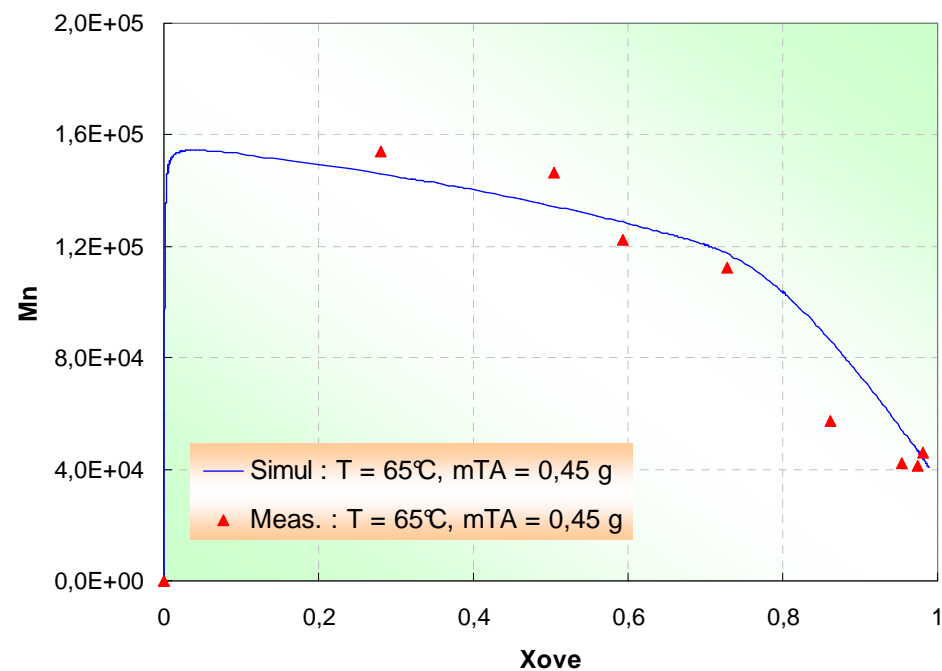
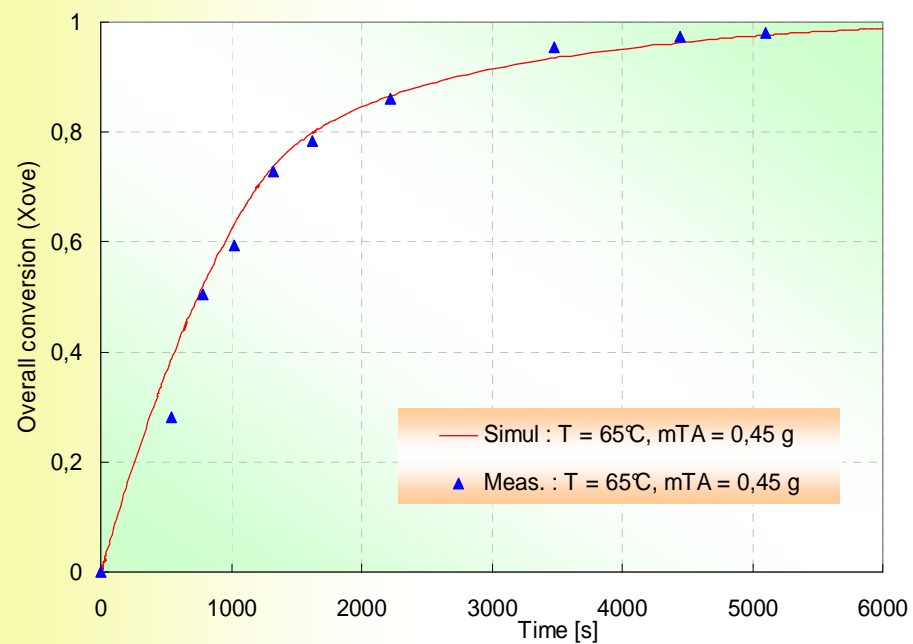
Objective function :

$$\begin{aligned}
 J = & w_X \cdot \ln \left(\sum_{\text{data}} (X_{\text{exp}} - X_{\text{mod}})^2 \right) + w_{d_p} \cdot \ln \left(\sum_{\text{data}} (d_{\text{pexp}} - d_{\text{pmod}})^2 \right) \\
 & + w_{\bar{M}_n} \cdot \ln \left(\sum_{\text{data}} (\bar{M}_{\text{nexp}} - \bar{M}_{\text{nmod}})^2 \right) + w_{\bar{M}_w} \cdot \ln \left(\sum_{\text{data}} (\bar{M}_{\text{wexp}} - \bar{M}_{\text{wmod}})^2 \right) + \\
 & w_{Fr_1} \cdot \ln \left(\sum_{\text{data}} (Fr_{1\text{exp}} - Fr_{1\text{mod}})^2 \right)
 \end{aligned}$$

Parameter identification results



Validation results



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General Context

Problematics : Simultaneous optimization of criteria often **conflicting** (productivity, cost, quality, security, environment...)



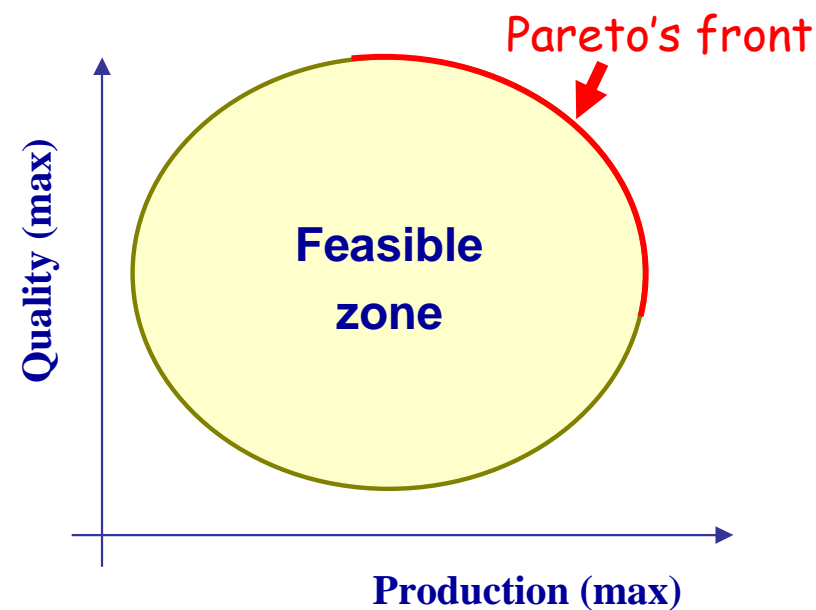
No optimal solution



Search for a group of compromises



Choice of the best compromise



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Definition of the problem :

$$\text{Min } f = [f_1, f_2]$$

$$f_1 = \frac{1}{t_{fc} - t_0} \int_{t_{fc}}^{t_0} |T_g - T_{g1}| dt + \frac{1}{t_{fs} - t_{fc}} \int_{t_{fs}}^{t_{fc}} |T_g - T_{g2}| dt$$

$$f_2 = -X(t_f)$$

s.t

$$\dot{x} = f(x(t), u(t), p, t)$$

$$\frac{1}{t_{fc} - t_0} \int_{t_{fc}}^{t_0} (X_a - X(t))^2 dt \leq \varepsilon^2$$

$$u_{\text{inf}} \leq u \leq u_{\text{sup}}$$



u: feed rate (Q_f)

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Conclusions

Elaboration and validation of a tendency model able to predict :

Overall and partial conversions

Residual monomers

Number and weight average molecular weights

Particles diameters

Development of a methodology to solve multiobjective decision problems :

Simultaneous optimization of several criteria

Productivity

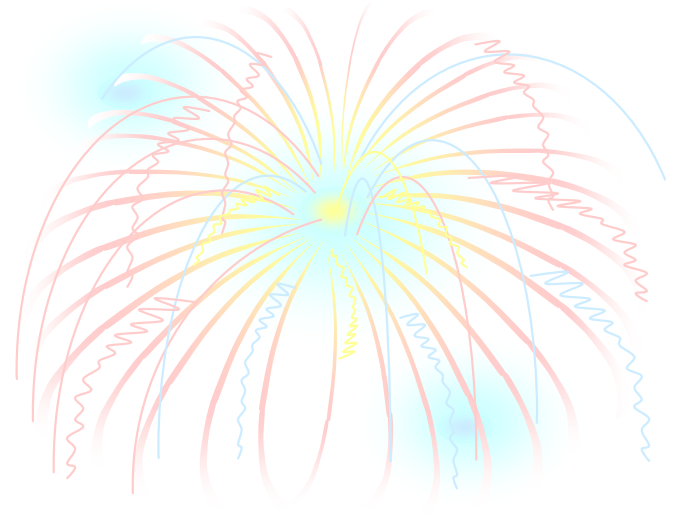
Quality

Futur trends

Decision-making support

Implementation of a solution from Pareto's front

Dynamic optimization (one criterium)



THANK YOU

ĎAKUJEM